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NOISE IMPACT ASSESSMENT REPORT - KITCHEN EXTRACTION SYSTEM

94 WHITLEY STREET, READING RG2 0EQ

FOR

GOYA WORKS

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The preparation of this report by Sound Licensing Ltd. has been undertaken within the terms of the proposal using all reasonable skill and care. Sound Licensing Ltd accepts no responsibility for the data provided by other bodies and no legal liability arising from the use by other persons of data or opinions contained in this report.

1. EXECUTIVE SUMMARY

The Client intends to seek planning approval for the installation of mechanical plant (Kitchen Extraction System) to service the premises at 94 Whitley Street, Reading RG2 0EQ.

Sound Licensing has undertaken an environmental noise survey at the site in order to determine prevailing background noise levels that are representative of the nearest noise sensitive properties, which have been identified as the residential premises at 92 Whitley Street, RG2, and the residential premises above the site at 94 Whitley Street.

The results of the noise survey are considered reasonable given the location of the measurement position and the existing noise sources in the local vicinity.

Noise calculations of the mechanical plant have been undertaken using all available details and plans provided by the client and obtaining manufacturers' specifications wherever possible. The data and information form the basis of the assessment.

Noise break-out limits for the mechanical plant have been proposed based on the methodologies of British Standard (BS) 4142:2014+A1:2019 and in accordance to Local Authority policy. A robust, worst-case assessment of the noise levels associated to the proposed mechanical plant has been undertaken.

In accordance with BS 4142:2014+A1:2019 guidance, the predicted noise impact due to the operation of the mechanical plant ***"is an indication of the specific sound source having a low impact"***. The predicted noise level of the mechanical plant at the nearest noise sensitive properties is considered to comply with the Reading Borough Council's policy.

2. INTRODUCTION

The client is proposing to install a new kitchen extraction system at the rear of 94 Whitley Street, Reading RG2 0EQ, the noise from which could have the potential to affect existing noise sensitive properties nearby.

The purposes of this report are:

- To determine prevailing environmental noise levels affecting surrounding properties due to nearby noise sources (e.g. road traffic, aircraft etc);
- Based on the above, to present noise emission limits in accordance with the requirements of BS 4142:2014+A1:2019 and Local Authority policy, and
- To undertake an assessment to demonstrate compliance with the Local Authority noise requirements.

3. SITE DESCRIPTION

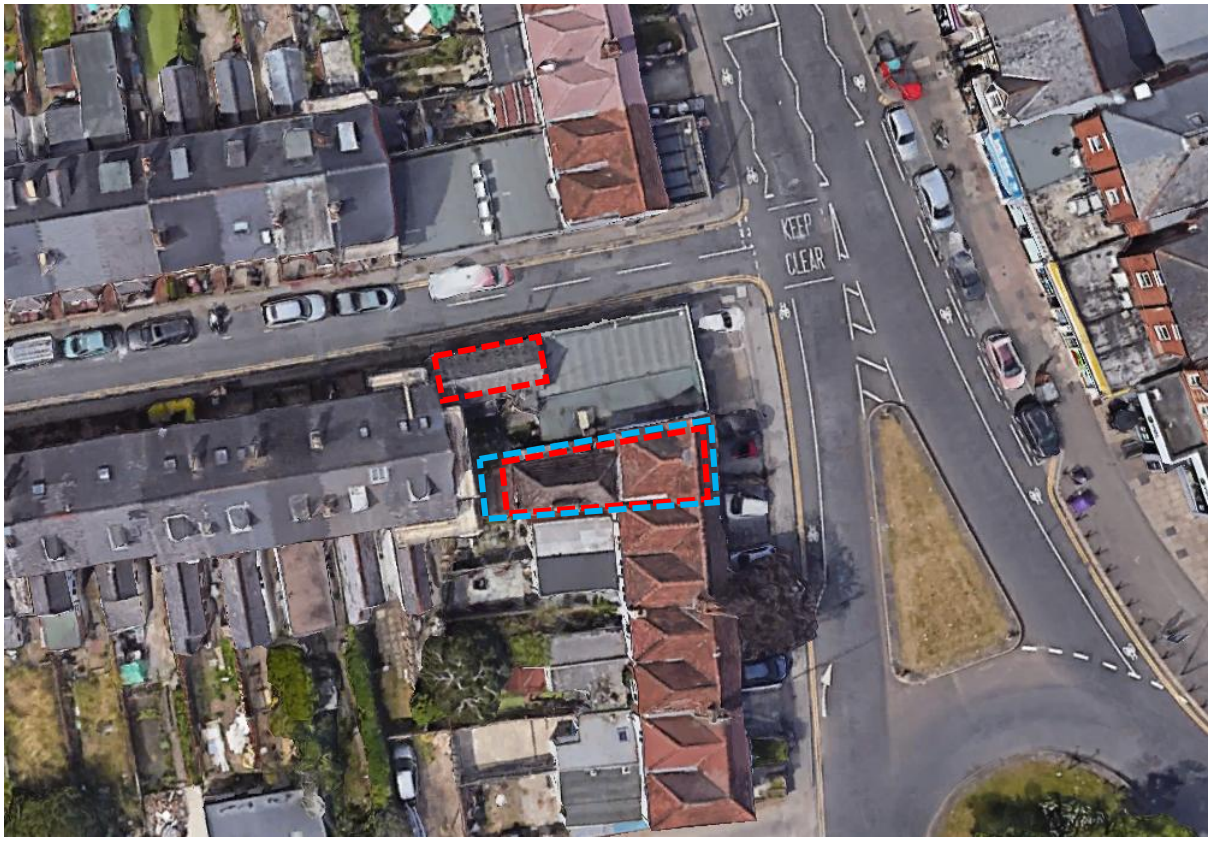
Planning permission is being sought for the installation of mechanical plant (Kitchen Extraction System) at 94 Whitley Street, Reading RG2 0EQ (hereafter referred to as 'the site'). The property is a traditionally built two-storey terraced building in the Borough of Reading. It is located in a mixed area comprising predominantly of commercial units at ground floor level with residential accommodation on the floors above.

The nearest sensitive residential receptors were noted to be the first-floor window located on the rear/side façade of 92 Whitley Street, RG2, with a clear line of sight, at an approximate distance of 5m from the discharge point of the flue and the first-floor side façade window at 94 Whitley Street, with building screening, at an approximate distance of 6m.

The nearest sensitive receptors are identified in figure 3.1. If the noise impact assessment details that there is an indication of the specific sound source having a low impact at these premises then it can be safely assumed it will be met at other properties of equal distance and/or those further away.

Figure 3.1 shows the site highlighted in **blue** with the nearest noise sensitive premises highlighted in **red**.

Figure 3.1 Site Location and Surrounding Land Use



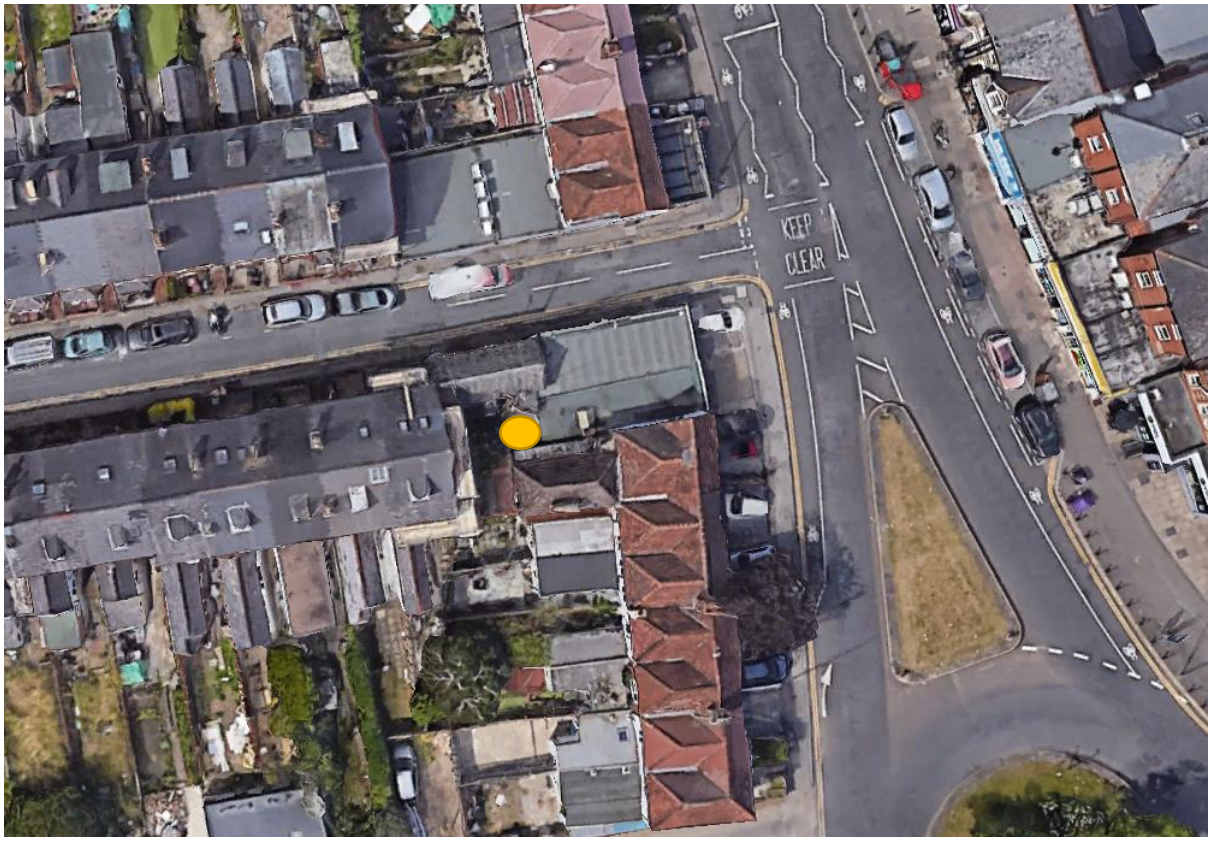
Source: Google Maps

4. ENVIRONMENTAL NOISE SURVEY METHODOLOGY

An unmanned environmental noise survey was undertaken at a single measurement location at first floor level to the side of the site. The survey was undertaken between 12:00 hours on the 9th June and 11:45 hours on the 11th June 2026. A survey at this time covers the most sensitive period of time in which the mechanical plant system may be operational.

Ambient, background and maximum noise levels (L_{Aeq}, L_{A90} and L_{Amax} respectively) were measured throughout the noise survey in continuous 15-minute periods. The approximate measurement position is indicated in **orange** on Figure 4.1 below.

Figure 4.1 Site Plan Showing Approximate Location of Measurement Position



Source: Google Maps

The sound level meter microphone was positioned on a tripod at a height of 1.5 metres, 1 metre from the side façade of the building at first-floor level. The position is not considered to be in free-field and therefore a -3dB façade correction will be applied. The monitoring position is considered representative of background noise levels at the nearest identified noise sensitive properties. The monitoring position was chosen for equipment security reasons also.

The equipment used for the noise survey is summarised in Table 4.1.

Table 4.1 Description of Equipment used for Noise Survey

Equipment	Description	Quantity	Serial Number
Larson Davis Sound Expert LxT	Type 1 automated logging sound level meter	1	0003739
Larson Davis 377B02	½" microphone	1	308849
Larson Davis	Pre-amplifier	1	028021
Larson Davis CAL200	Class 1 Calibrator	1	12245

The noise survey and measurements were conducted in accordance with BS7445-1:2003 '*Description and measurement of environmental noise. Guide to quantities and procedures*'.

Weather conditions throughout the entire noise survey period were noted to be mild (approx. 6-18° Celsius), broken clouds (20 to 70% cloud cover approximately) with a light wind (<5m/s). These weather conditions were checked against and confirmed by the use of the Met Office mobile application available on smart phone technology. These conditions were maintained throughout the majority of the survey period and are considered reasonable for undertaking environmental noise measurements.

The noise monitoring equipment was field calibrated before and after the noise survey period. No significant drift was recorded (±0.3 dB). Equipment calibration certificates can be provided upon request.

5. NOISE SURVEY RESULTS AND OBSERVATIONS

5.1 Results

A summary of the measured ambient and typical background noise levels during the proposed operational hours are shown in Table 5.1 below (full monitoring data can be found in Appendix C).

Table 5.1 Measured Ambient and Typical Background Sound Pressure Levels

Date / Period (hours)	Ambient Sound Pressure Level, dB $L_{Aeq,1hour}$*	Typical Background Sound Pressure Level, dB $L_{A90,1hour}$*
09/06/2026 (12:00 to 23:00)	47-53	46
10/06/2026 (09:00 to 23:00)	49-56	44
11?06/2026 (09:00 to 11:45)	53-54	49

*Façade correction -3dB.

The typical background noise level at the measurement position during the survey, at the time in which the plant could be operational, is **44dB** $L_{A90,1hour}$.

5.2 Observations

Given that the noise survey was unmanned, noise sources could not be identified. However, at the beginning and end of the survey background noise was dominated by noise from the vehicles on the local road network. After analysis of the data no significant abnormal noise source(s) were identifiable. It is considered that the measured noise levels are reasonable given the location of the measurement position.

6. EXTERNAL NOISE EMISSION LIMITS

6.1 Local Authority Requirements

The site lies within the jurisdiction of the Reading Borough Council. The following criteria has previously been provided by the local authority:

'The assessment shall be carried out for in accordance with BS4142:2014+A1:2019 methodology. The predicted specific sound level (LAeq,TR) (with reference to BS4142) as measured at a point 1 metre external to the nearest noise-sensitive façade shall be at least 10dB below the pre-existing background sound level, LA90,T when all plant/equipment (or any part of it) is in operation. The predicted rating level, LAr,Tr (specific sound level plus any adjustment for the characteristic features of the sound as measured at a point 1 metre external to the nearest noise-sensitive façade (habitable window of a dwelling) shall not exceed the pre-existing background sound level, LA90,T, when all plant/equipment (or any part of it) is in operation.'

For the purposes of this report, an assessment has been undertaken in line with BS 4142:2014+A1:2019. A design criterion of achieving a minimum 10dB(A) below the typical background noise level has been adopted in line with the Local Authorities policy. Taking the noise monitoring data in Section 5 and Local Authority requirements above, the following design target has been adopted for mechanical plant as provided in Table 6.1.

Table 6.1 Maximum Noise Emission Design Target at Residential Premises

Date / Period (hours)	Typical Background Sound Pressure Level, dB $L_{A90,1hour}$*	Rating Noise Level at 1m from Nearest Residential Facade, dB $L_{Ar,T}$
09/06/2026 – 11/06/2026 (12:00 to 11:45)	44	34

* Façade correction -3dB

6.2 BS 4142:2014+A1:2019

BS 4142:2014+A1:2019 "Methods for rating and assessing industrial and commercial sound" presents a method for assessing the significance and possible adverse impact due to an industrial noise source, based on a comparison of the source noise levels and the background noise levels, both of which are measured or predicted at a noise sensitive receiver e.g. a residential property.

The specific noise level due to the source is determined, with a series of corrections for tonality, impulsivity, intermittency or other unusual characteristic. The rating level is then compared to the background noise level and the significance of the new noise source likelihood of any adverse impact is determined in accordance with the following advice:

"The significance of sound of an industrial and/or commercial nature depends upon both the margin by which the rating level of the specific sound source exceeds the background sound level and the context in which the sound occur. A difference of around +10 dB or more is likely to be an indication of a significant adverse impact, depending on the context. A difference of around +5 dB is likely to be an indication of an adverse impact, depending on the context. The lower the rating level is relative to the measured background sound level, the less likely it is that the specific sound source will have an adverse impact or a significant adverse impact. Where the rating level does not exceed the background sound level, this is an indication of the specific sound source having a low impact, depending on the context."

7. PROPOSED KITCHEN EXTRACTION SYSTEM AND ASSOCIATED NOISE LEVELS

It is proposed to install the following items of plant at the rear of the premises.

Table 7.0 Proposed Kitchen Extraction Fan Motor

External Plant Item	Make	Model	Reference Noise Level* $L_{w(A)}$
Kitchen Extract Fan Motor	Helios	GBW 450/4	Outlet 75dB

*Reference sound power levels. Manufacturer's specifications are provided in Appendix B.

The ducting will be 450mm standard circular duct work. The extraction fan motor will be located internally and therefore only noise from the duct terminus has been considered.

In reference to section 6 of this report, no penalty addition has been applied for intermittency as with proposed mitigation, the system will be not be readily distinguishable against the residual acoustic environment. Penalty additions have not been applied for tonality as manufacturers' data shows no significant characteristics, or for impulsiveness as it is considered that these characteristics will not be perceptible sufficient to attract attention at the noise receptors. Penalty additions have not been applied for any other sound characteristics as mechanical plant of this type generally do not demonstrate such features.

7.1 Silencer

The extraction system will be fitted with a CP03-CAP-0450-2D Acoustica silencer and a CP03-CA-0450-1D Acoustica silencer on the atmosphere side of the fan. The silencers provide the attenuation shown in Table 7.1. All silencers should be Melinex lined.

Table 7.1 Silencer Attenuation

Silencer	125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	8kHz
CP03-CAP-0450-2D	7	12	22	29	29	25	20
CP03-CA-0450-1D	3	6	12	13	11	9	7

7.2 Directivity

A directivity correction should be applied as the extract fan duct aperture is to terminate approximately 90˚ to the residential window at 92 Whitley Street and 120˚ to the residential window at 94 Whitley Street. A duct opening of 450mm has been used. The levels of attenuation (dB) at each octave frequency band (Hz) are provided in table 7.2 below.

Table 7.2 Directivity Attenuation

	125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	8kHz
90˚	0	2	6	7	14	16	19
120˚	2	5	10	13	20	22	22

Little Red Book of Acoustics (Fourth Edition 2024)

7.3 Building Screening

Due to the positioning of the mechanical plant, there will be significant building screening from the duct terminus to the residential window on the side façade of 94 Whitley Street, so there will be no direct line of sight, therefore attenuation due to barrier loss has also been considered (calculations are provided in Appendix D).

Corrections have also been applied for the attenuation from duct bends (1)*.

* Reference: Improving Ductwork, EU project, Brussls 1999. Also same as CIBSE.

8. NOISE IMPACT ASSESSMENT

This section presents calculations to predict the noise impact of the proposed kitchen extraction system, located at the site, at the nearest noise sensitive properties.

8.1 Proposed Operational Hours and Background Noise Levels

The kitchen extraction system will operate as required during the operating hours of the proposed business. The opening hours are from 09:00 - 23:00 hours Monday to Sunday.

The typical background noise level at the measurement position during the survey is **44dB** $L_{A90,1hour}$. The design range is **34dB** $L_{Ar,T}$ at 1m from the façade of the nearest residential premises.

8.2 Nearest Noise Sensitive Properties

The nearest sensitive residential receptors were noted to be the first-floor window located on the rear/side façade of 92 Whitley Street, RG2, with a clear line of sight, at an approximate distance of 5m from the discharge point of the flue and the first-floor side façade window at 94 Whitley Street, with building screening, at an approximate distance of 6m.

8.3 Description of Calculation Process

In accordance with the methodologies of BS 4142:2014+A1:2019, calculations have been undertaken to predict noise levels in which the kitchen extraction system could be operational at its maximum level. Given the distances between the noise sources and the noise sensitive receptors, point source calculations have been used.

8.4 Noise Level Predictions

Calculations to predict the noise of the kitchen extraction system operating at the facade of the residential property is given below. Full calculations are provided in Appendix D.

The rating noise level at 1m from the residential window at 92 Whitley Street, with the mechanical plant operating, is predicted to be **33dB $L_{Aeq,T}$** which is **11dB(A) below** the typical background noise level (44dB $L_{A90,1hour}$).

The rating noise level at 1m from the residential window at 94 Whitley Street, with the mechanical plant operating, is predicted to be **19dB $L_{Aeq,T}$** which is **25dB(A) below** the typical background noise level (44dB $L_{A90,1hour}$).

In accordance with BS 4142:2014+A1:2019 guidance, noise from the mechanical plant ***"is an indication of the specific sound source having a low impact"***. *The lower the rating level is relative to the measured background level, the less likely it is that the specific sound source will have an adverse impact.*

8.5 Vibration

In addition to the control of airborne noise transfer, it is important to consider the transfer of noise as vibration to adjacent properties as well as any sensitive areas of the same building. Vibration from the system is not expected, however, as a precaution plant should wherever possible be installed on suitable type isolators. The fan should be installed with flexible connections to adjacent structures.

Uncertainty

The levels of uncertainty in the data and calculations are considered to be low given the robust exercise undertaken in noise monitoring and the confidence in the data statistical analysis. Manufacturers' data for the plant is highly likely to be robust. Detailed calculations and resultant noise levels at the residential location are considered to be confidently predicted.

9. CONCLUSION

The Client intends to seek planning approval for the installation of mechanical plant (Kitchen Extraction System) to service the premises at 94 Whitley Street, Reading RG2 0EQ.

Sound Licensing has undertaken an environmental noise survey at the site in order to determine prevailing background noise levels that are representative of the nearest noise sensitive properties.

The operation of the kitchen extraction system, in accordance with BS 4142:2014+A1:2019 guidance, indicates to creating a low impact. All worst-case scenarios have been applied to the assessment.

The predicted operating noise level of the kitchen extraction system is demonstrated to comply with the Borough of Reading Council's policy.

APPENDIX A – Acoustic Terminology

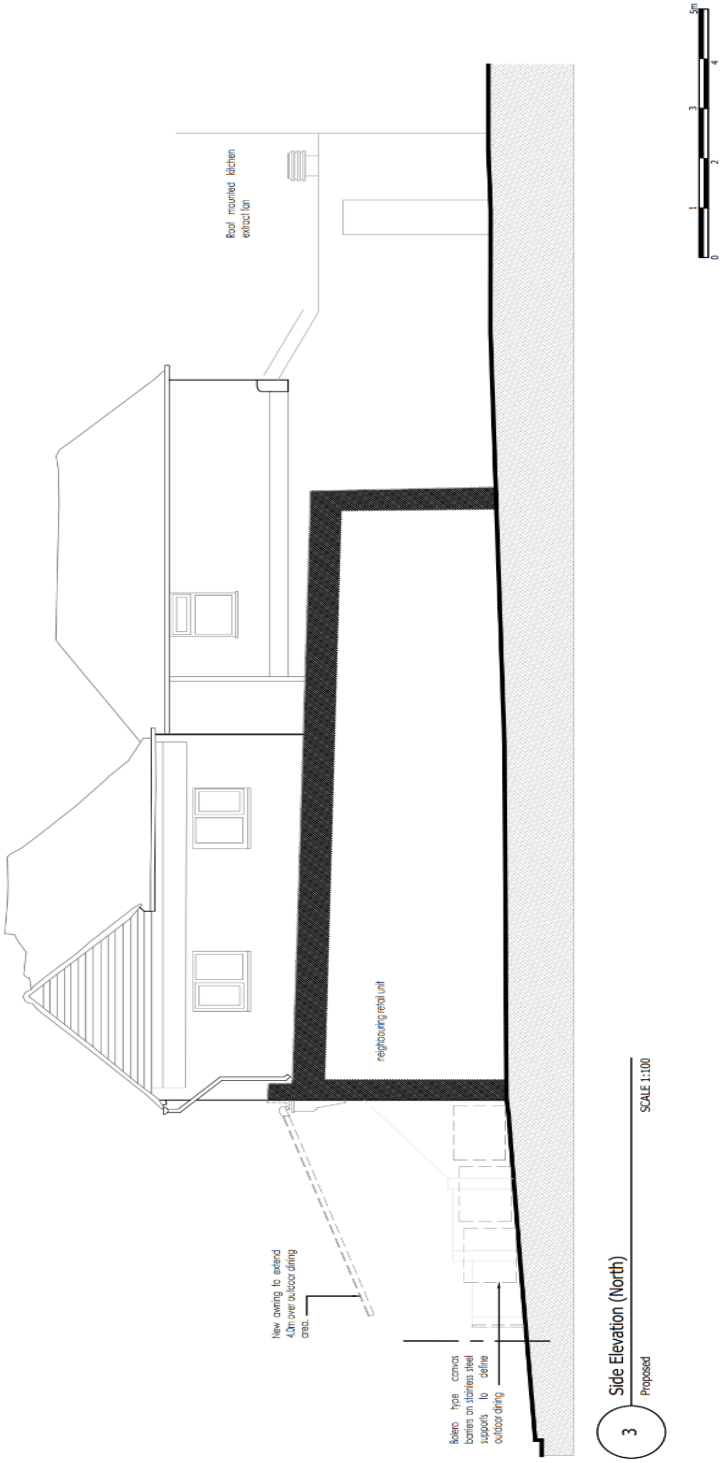
Parameter	Description
Acoustic environment	Sound from all sound sources as modified by the environment
Ambient sound	Totally encompassing sound in a given situation at a given time, usually composed of sound from many sources near and far
Ambient sound level, La = LAeq,T	Equivalent continuous A-weighted sound pressure level of the totally encompassing sound in a given situation at a given time, usually from many sources near and far, at the assessment location over a given time interval, T
Background sound level, LA90,T	A-weighted sound pressure level that is exceeded by the residual sound at the assessment location for 90% of a given time interval, T, measured using time weighting F and quoted to the nearest whole number of decibels
Decibel (dB)	A logarithmic scale representing the sound pressure or power level relative to the threshold of hearing ($20x10^{-6}$ Pascals).
Equivalent continuous A-weighted sound pressure level, LAeq,T	Value of the A-weighted sound pressure level in decibels of continuous steady sound that, within a specified time interval, T = t2 – t1, has the same mean-squared sound pressure as a sound that varies with time
Measurement time interval, Tm	Total time over which measurements are taken
Rating level, LAr,Tr	Specific sound level plus any adjustment for the characteristic features of the sound
Reference time interval, Tr	Specified interval over which the specific sound level is determined
Residual sound	Ambient sound remaining at the assessment location when the specific sound source is suppressed to such a degree that it does not contribute to the ambient sound
Residual sound level, Lr = LAeq,T	Equivalent continuous A-weighted sound pressure level of the residual sound at the assessment location over a given time interval, T
Specific sound level, Ls = LAeq,Tr	Equivalent continuous A-weighted sound pressure level produced by the specific sound source at the assessment location over a given reference time interval, Tr
Specific sound source	Sound source being assessed

References:

BS 4142:2014+A1:2019 'Methods for rating and assessing industrial and commercial sound'
Blue Tree Acoustics 2024 'Little Red Book of Acoustics (Fourth Edition)'

APPENDIX B – Data Sheets and Figures

Proposed Side Elevation



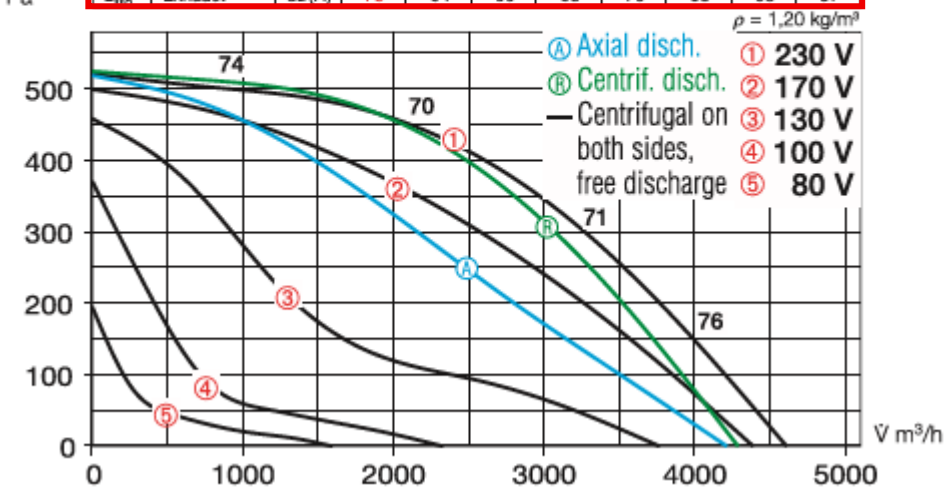
Helios GBW 450/4 – Proposed Kitchen Extraction Fan Motor

GB

Arbitrary installation position and flexible assembly by five possible discharge directions.

GBW 450/4

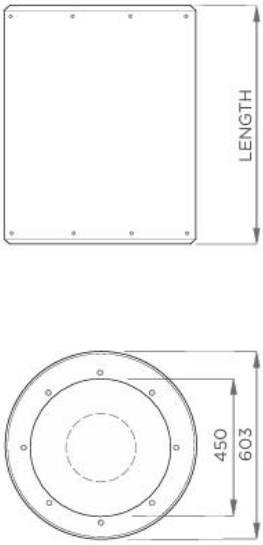
Frequency		Hz	Total	125	250	500	1k	2k	4k	8k
L_{WA}	Case breakout	dB(A)	60	56	56	51	47	44	39	31
L_{WA}	Intake	dB(A)	69	61	63	65	67	65	60	54
L_{WA}	Exhaust	dB(A)	75	64	66	68	70	68	63	57



Acoustica CAP-0450-2D and CA-0450-1D – Proposed Silencers

ACOUSTICA™

CP03-CA-0450 SILENCER



PATTERN A - 8 x M10 - 500 PCD
PATTERN B - 12 x M8 - 487 PCD

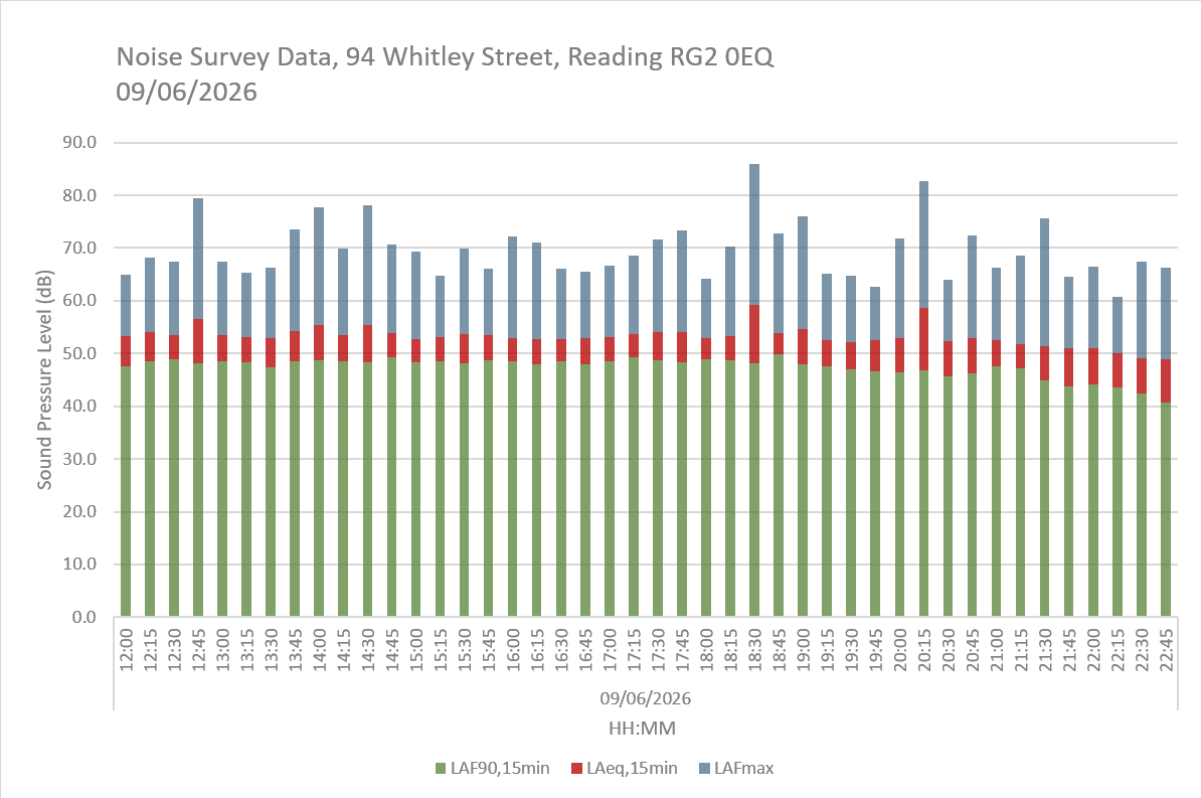
INSERTION LOSS (dB) - CENTRE BAND FREQUENCY

DIMENSIONAL DATA

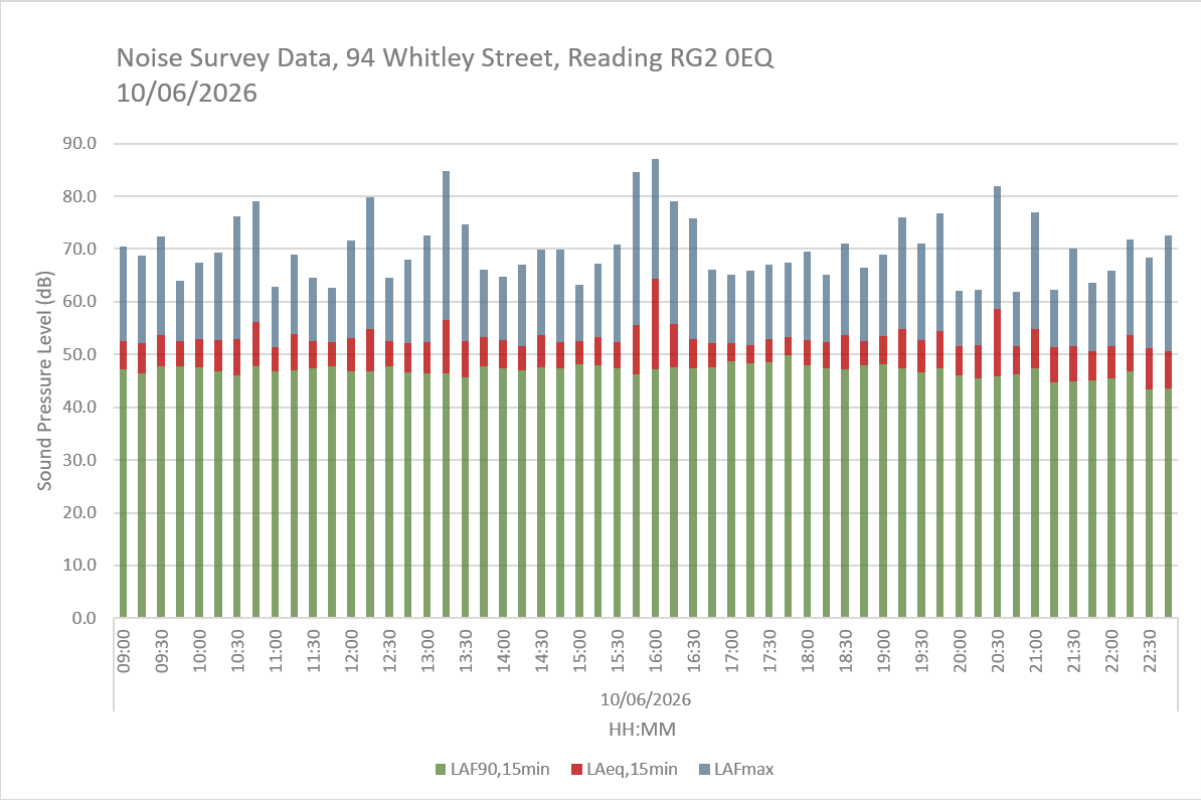
PRODUCT CODE	63 Hz	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz	8000 Hz	LENGTH	MASS
CP03-C*-0450-1D	2	3	6	12	13	11	9	7	450mm	15 Kg
CP03-C*-0450-2D	3	4	8	17	18	15	11	10	900mm	27 Kg
CP03-C*P-0450-1D	2	6	8	16	23	23	21	16	450mm	18 Kg
CP03-C*P-0450-2D	3	7	12	22	29	29	25	20	900mm	32 Kg

Replace " in code with A or B for connection pattern. Insertion loss data is derived from continual testing to BS4718 and other standards in independent UKAS certified laboratories, which includes where appropriate, re-generated or self noise testing in both forward and reverse flow conditions. If you request system analysis from our technicians all predictions will be assessed using the relevant certified insertion loss data together with relevant dynamic corrections.

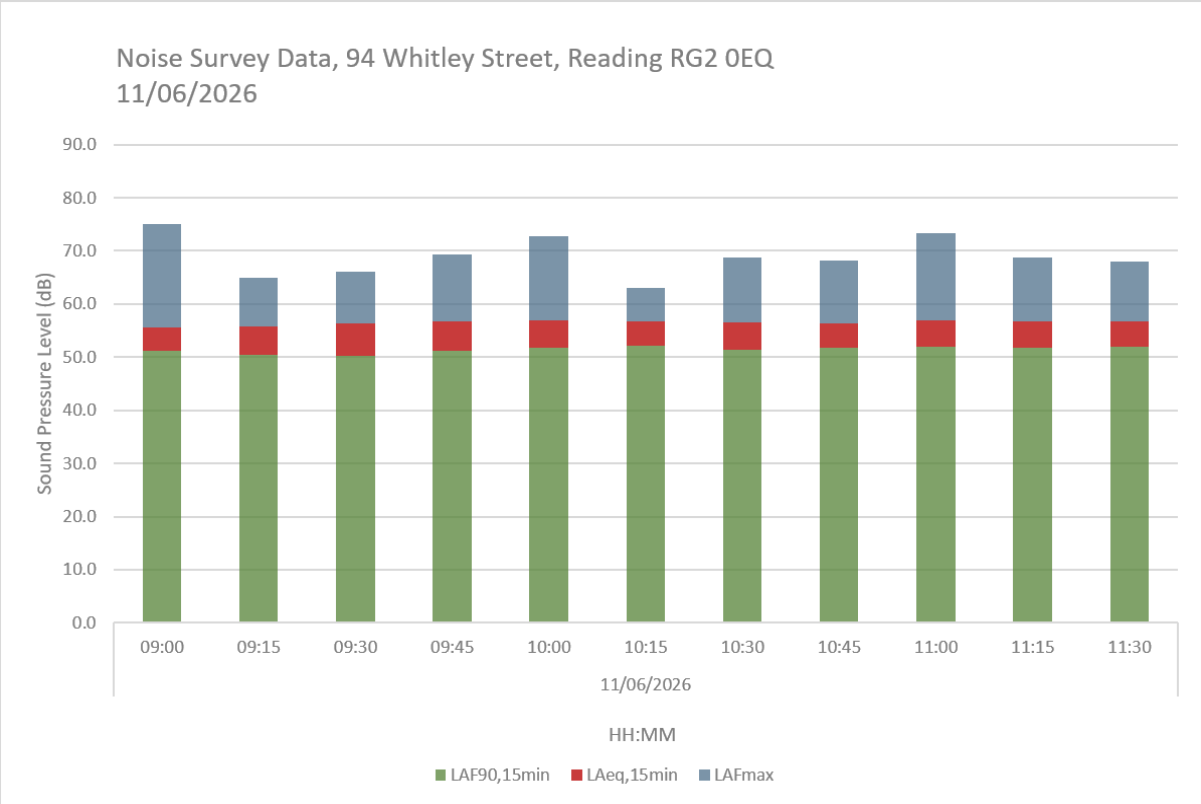
APPENDIX C – Noise Monitoring Data



Date	Time	$L_{Aeq,15min}$	L_{AFmax}	$L_{AF90,15min}$	$L_{Aeq,1hour}$	$L_{AF90,1hour}$	Date	Time	$L_{Aeq,15min}$	L_{AFmax}	$L_{AF90,15min}$	$L_{Aeq,1hour}$	$L_{AF90,1hour}$
09/06/2026	12:00	53.3	65.0	47.6	54.5	48.4	09/06/2026	18:00	53.0	64.2	48.9	55.7	48.9
	12:15	54.0	68.2	48.6				18:15	53.2	70.2	48.7		
	12:30	53.4	67.5	48.9				18:30	59.2	86.0	48.2		
	12:45	56.5	79.4	48.2				18:45	53.8	72.7	49.8		
	13:00	53.5	67.4	48.6	53.5	48.2		19:00	54.6	76.0	48.0	53.1	47.4
	13:15	53.1	65.3	48.3				19:15	52.6	65.1	47.6		
	13:30	53.0	66.2	47.4				19:30	52.2	64.7	47.0		
	13:45	54.3	73.5	48.5				19:45	52.5	62.7	46.7		
	14:00	55.4	77.7	48.8	54.6	48.7		20:00	52.9	71.8	46.4	55.1	46.3
	14:15	53.4	69.9	48.5				20:15	58.7	82.7	46.8		
	14:30	55.3	78.0	48.3				20:30	52.4	63.9	45.7		
	14:45	53.8	70.7	49.2				20:45	52.9	72.3	46.3		
	15:00	52.7	69.4	48.4	53.2	48.5		21:00	52.5	66.2	47.5	51.7	46.1
	15:15	53.1	64.7	48.6				21:15	51.7	68.5	47.2		
	15:30	53.7	69.9	48.2				21:30	51.3	75.7	44.9		
	15:45	53.4	66.0	48.8				21:45	51.0	64.5	43.8		
	16:00	53.0	72.2	48.6	52.9	48.3		22:00	51.0	66.5	44.2	49.8	42.9
	16:15	52.8	71.0	48.0				22:15	50.0	60.8	43.6		
	16:30	52.8	66.1	48.5				22:30	49.1	67.4	42.5		
	16:45	52.9	65.5	47.9				22:45	48.9	66.2	40.7		
	17:00	53.1	66.6	48.6	53.7	48.7							
	17:15	53.6	68.6	49.2									
	17:30	54.0	71.7	48.8									
	17:45	54.1	73.3	48.3									



Date	Time	$L_{Aeq,15min}$	L_{AFmax}	$L_{AF90,15min}$	$L_{Aeq,1hour}$	$L_{AF90,1hour}$	Date	Time	$L_{Aeq,15min}$	L_{AFmax}	$L_{AF90,15min}$	$L_{Aeq,1hour}$	$L_{AF90,1hour}$
10/06/2026	09:00	52.6	70.4	47.1	52.8	47.3	10/06/2026	16:00	64.4	87.0	47.1	59.4	47.4
	09:15	52.2	68.7	46.5				16:15	55.7	79.0	47.5		
	09:30	53.7	72.4	47.8				16:30	53.0	75.8	47.3		
	09:45	52.5	63.9	47.7				16:45	52.1	66.0	47.6		
	10:00	52.9	67.4	47.5	53.9	47.1		17:00	52.2	65.2	48.7	52.6	48.9
	10:15	52.8	69.4	46.9				17:15	51.8	65.9	48.3		
	10:30	52.9	76.2	46.1				17:30	53.0	67.0	48.5		
	10:45	56.1	79.1	47.8				17:45	53.3	67.4	49.8		
	11:00	51.4	62.9	46.8	52.6	47.2		18:00	52.8	69.5	48.0	52.9	47.6
	11:15	53.8	69.0	47.0				18:15	52.3	65.2	47.3		
	11:30	52.5	64.5	47.3				18:30	53.7	71.0	47.2		
	11:45	52.4	62.6	47.8				18:45	52.5	66.5	48.0		
	12:00	53.1	71.7	46.9	53.3	47.0		19:00	53.5	68.9	48.1	54.0	47.4
	12:15	54.8	79.9	46.9				19:15	54.9	75.9	47.3		
	12:30	52.6	64.6	47.7				19:30	52.8	71.1	46.6		
	12:45	52.2	67.9	46.6				19:45	54.5	76.8	47.4		
	13:00	52.3	72.5	46.4	54.0	46.6		20:00	51.5	62.1	46.1	54.6	45.9
	13:15	56.5	84.8	46.4				20:15	51.7	62.3	45.5		
	13:30	52.6	74.6	45.6				20:30	58.6	81.9	45.8		
	13:45	53.3	66.1	47.7				20:45	51.5	61.8	46.3		
	14:00	52.7	64.8	47.3	52.6	47.3		21:00	54.9	76.9	47.3	52.5	45.6
	14:15	51.6	67.0	47.0				21:15	51.4	62.3	44.7		
	14:30	53.7	69.9	47.6				21:30	51.5	70.1	44.9		
	14:45	52.3	69.8	47.3				21:45	50.7	63.5	45.0		
	15:00	52.5	63.3	48.2	53.6	47.5		22:00	51.5	65.8	45.4	51.9	45.0
	15:15	53.2	67.3	47.9				22:15	53.7	71.8	46.8		
	15:30	52.4	70.9	47.4				22:30	51.2	68.3	43.4		
	15:45	55.6	84.5	46.3				22:45	50.7	72.6	43.6		



Date	Time	$L_{Aeq,15min}$	L_{AFmax}	$L_{AF90,15min}$	$L_{Aeq,1hour}$	$L_{AF90,1hour}$
11/06/2026	09:00	55.6	75.1	51.1	56.2	50.8
	09:15	55.7	65.0	50.5		
	09:30	56.4	66.1	50.2		
	09:45	56.8	69.4	51.2		
	10:00	57.0	72.7	51.8	56.7	51.8
	10:15	56.8	63.0	52.1		
	10:30	56.5	68.8	51.3		
	10:45	56.4	68.1	51.8		
	11:00	57.0	73.3	52.0	56.9	51.9
	11:15	56.8	68.7	51.8		
	11:30	56.8	68.0	51.9		

APPENDIX D – Calculations

92 Whitley Street

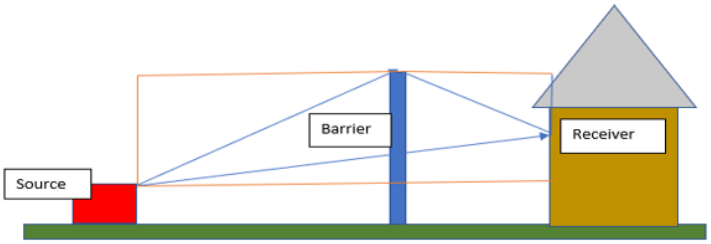
Attenuation per double distance required =			6	dB			Metres	
(6dB for LpA recommended)				Enter Distance =			4	
	Frequency Hz							
	125	**250**	**500**	**1000**	**2000**	**4000**	**8000**	Total
	80.1	74.6	71.2	70	66.8	62	58.1	82.08
Total LW	80.1	74.6	71.2	70.0	66.8	62.0	58.1	82.08
'A' Weight	16.1	8.6	3.2	0	-1.2	-1	1.1	
LWA (Power)	64.0	66.0	68.0	70.0	68.0	63.0	57.0	75.00
LPA at New Dist'	44.00	46.00	48.00	50.00	48.00	43.00	37.00	55.00
SILENCER	7	12	22	29	29	25	20	
SILENCER	3	6	12	13	11	9	7	
DUCT BENDS (1)	2	3	3	3	3	3	3	
DIRECTIVITY 90°	0	2	6	7	14	16	19	
LPA After Insert	**32.00**	**23.00**	**5.00**	**-2.00**	**-9.00**	**-10.00**	**-12.00**	**32.53**

Sound Pressure Level @ 1m from 92 Whitley Street = 33dB $L_{Ar,T}$

94 Whitley Street

Applicable where barrier breaks line of sight between source and receiver

Example Illustration of Barrier Attenuation



		Metres
Source to Barrier		2.4
Receiver to Barrier		3
Source to Receiver		5

Path Difference	0.4

Frequency Hz	63	125	250	500	1000	2000	4000	8000
Barrier Correction	7.7	9.5	11.7	14.2	17.0	19.8	22.8	25.8

Building Screening Attenuation Calculation

Attenuation per double distance required =			6	dB			Metres	
(6dB for LpA recommended)				Enter Distance =			5	
	Frequency Hz							
	125	250	500	1000	2000	4000	8000	Total
	80.1	74.6	71.2	70	66.8	62	58.1	82.08
Total LW	80.1	74.6	71.2	70.0	66.8	62.0	58.1	82.08
'A' Weight	16.1	8.6	3.2	0	-1.2	-1	1.1	
LWA (Power)	64.0	66.0	68.0	70.0	68.0	63.0	57.0	75.00
LPA at New Dist'	42.07	44.07	46.07	48.07	46.07	41.07	35.07	53.07
SILENCER	7	12	22	29	29	25	20	
SILENCER	3	6	12	13	11	9	7	
DUCT BENDS (1)	2	3	3	3	3	3	3	
BARRIER	9.5	11.7	14.2	17.0	19.8	22.8	25.8	
DIRECTIVITY 120°	2	5	10	13	20	22	22	
LPA After Insert	**18.61**	**6.41**	**-15.14**	**-26.89**	**-36.77**	**-40.71**	**-42.69**	**18.92**

Sound Pressure Level @ 1m from 94 Whitley Street = 19dB $L_{Ar,T}$